

New Design for the SARAF Phase II Linac

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SARAF: Soreq Applied Research Accelerator Facility

Driver: 40 MeV – 5mA proton/deuteron CW linac @ Soreq NRC, Israel

- Phase I of the linac was completed in 2009, it includes:
 - Ion Source: ECR capable of 8 mA – 20 keV/u beam
 - LEBT: Solenoid based with analyzing magnet
 - RFQ: 4-Rod CW 176 MHz - 1.5 MeV
 - MEBT: Simply a triplet for transverse matching
 - PSM: Prototype Superconducting Module with 6 HWRs & 3 Solenoids
- Current Status:
 - 1 mA – 3.5 MeV CW proton beam
 - 50 μ A – 4.7 MeV deuteron beam (Not CW due RFQ power limitation)
 - Preliminary experimental program & linac beam studies
- References:
 - L. Weissman et al “The Status of the SARAF Linac Project”, LINAC-2010
 - L. Weissman et al “First Experience at SARAF with Proton Beams”, DIPAC-09

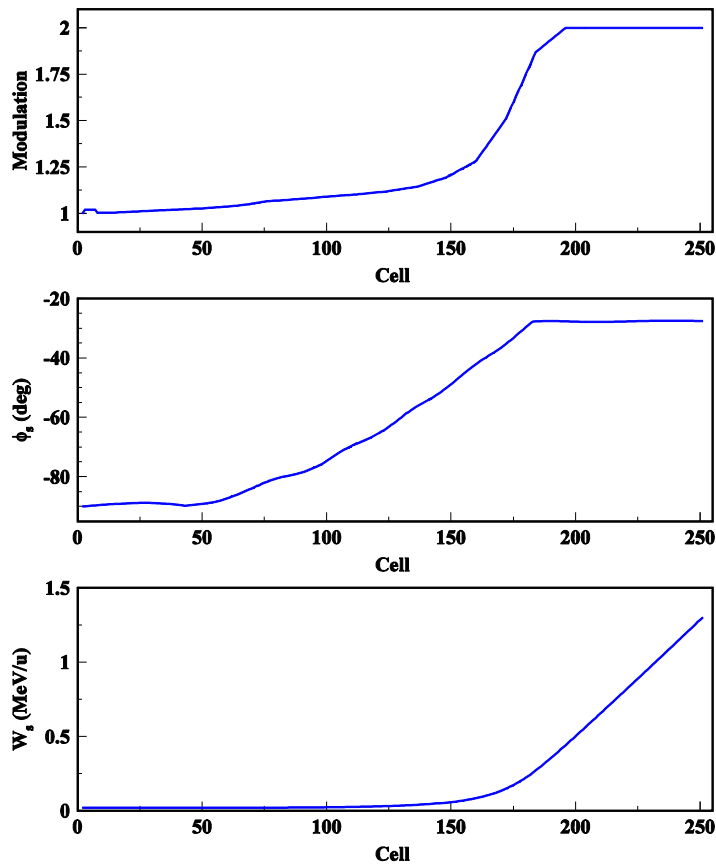
SARAF Phase II: Proposed Upgrades / Modifications

- Scope of Phase II
 - Additional Superconducting Accelerating Modules (SAMs).
 - Beam diagnostics instrumentation between and inside the SAMs.
 - RF control system for the SAMs.
 - Construction of an SRF facility at the SARAF site.
 - Upgrade or fix the existing SARAF RFQ.
- ANL's contribution so far
 - Design of an RFQ Upgrade
 - Optimized designs for RT rebunchers and new SC HWRs
 - New cryomodule design including all the components: Solenoids, Steerers, Cold BPMs, Alignment, Couplers, Tuners, ...
 - New linac layout based on the new cavity performance
 - End-to-end beam dynamics studies

176 MHz CW RFQ: General Design Parameters

Parameter	Value
Charge to mass ratio	1/2
Input energy, keV/u	20
Output energy, keV/u	1300
Frequency, MHz	176
Voltage, kV	75
Beam current design value, mA	5.0
RFQ length, m	3.8
Average radius, mm	4.4
Modulation factor, max	2.0
Min. aperture, mm	2.93
Min. transverse phase advance, degree	33.0
Transverse acceptance, norm, mm mrad	2.2
Maximum field at vane surface, Kilpatric units	1.6
Number of cells	250

176 MHz CW RFQ: Beam Dynamics Design

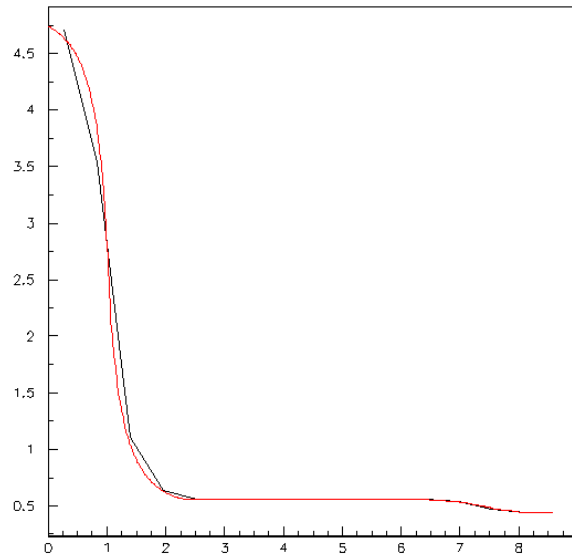


Beam	Proton	Deuteron
Input transverse emittance, rms, norm, mm·mrad	0.25	0.25
Input Twiss α	0.21	0.22
Input Twiss β , cm/rad	3.4	3.1
Transmission, %	99.7	99.9
Output longitudinal emittance, rms, keV/u·deg	36.6	36.3
Transverse rms emittance growth, %	0	0
Transverse 99% emittance growth, %	10	13
Particle loss inside the RFQ	$3 \cdot 10^{-3}$	$1 \cdot 10^{-3}$

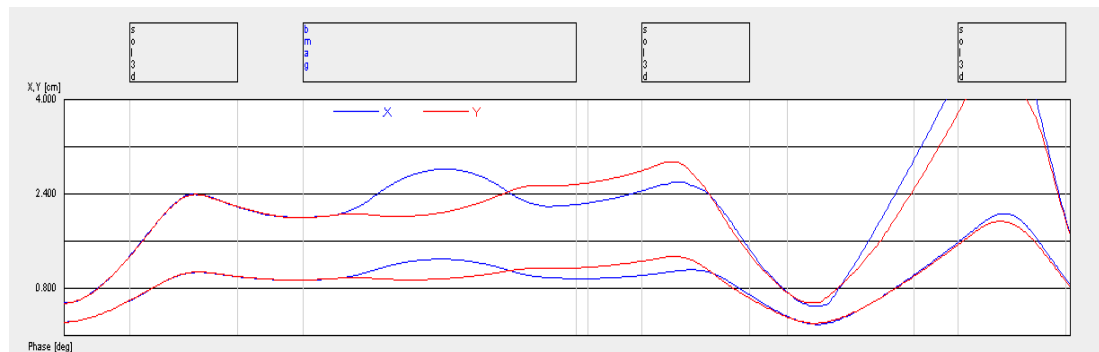
Two Important Design Features

- ✓ Almost 100% transmission to avoid contamination by deuteron breakup reactions
- ✓ A special input matcher to ease the matching and reduce emittance growth in the LEPT

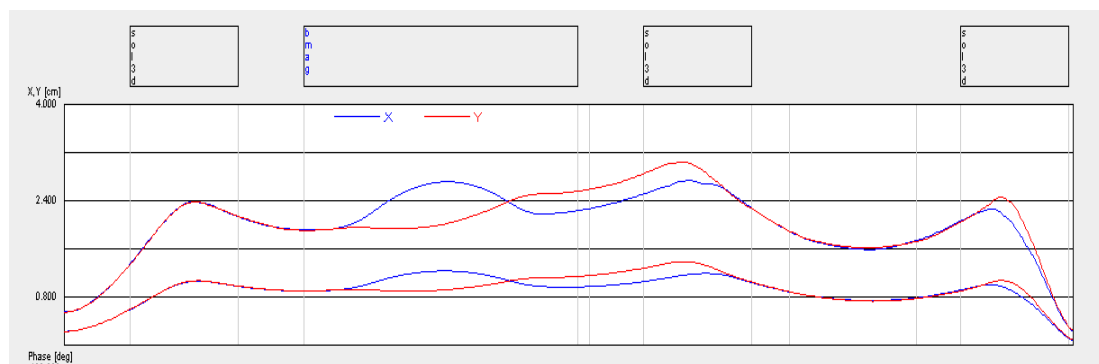
176 MHz CW RFQ: A Special Input Matcher



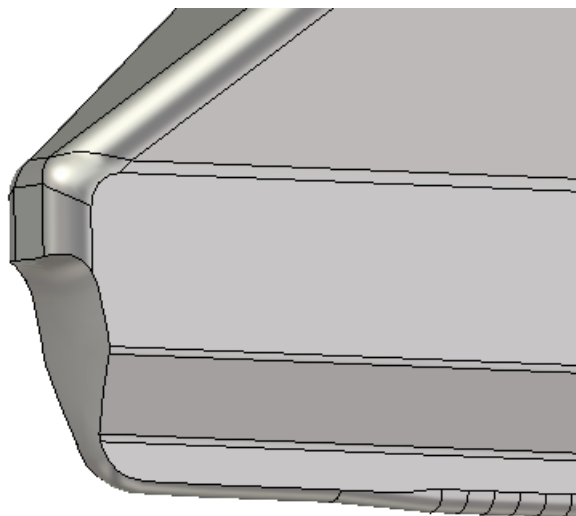
LEBT with original 6 cell input matcher: $\alpha \sim 1.5$



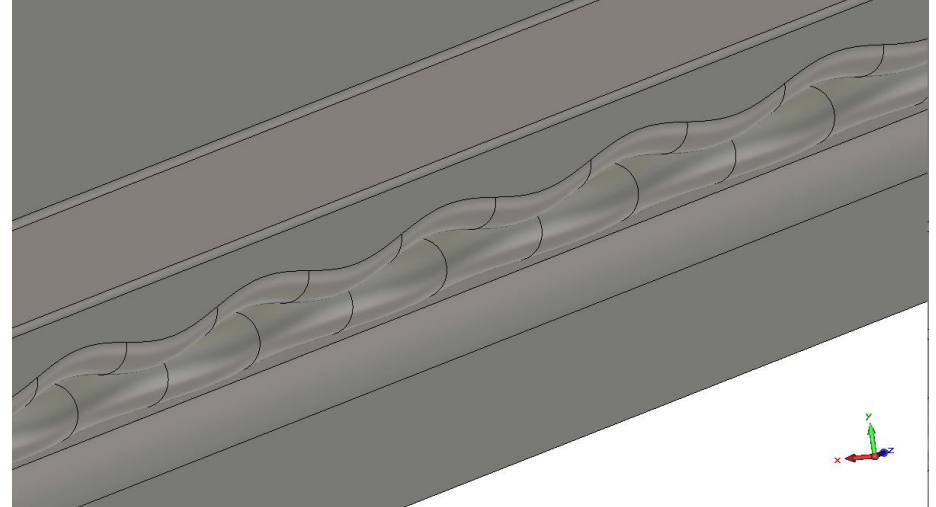
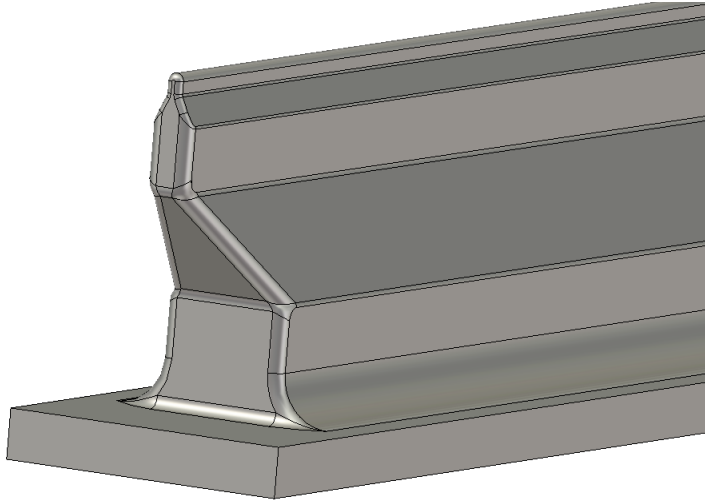
LEBT with special 15 cell input matcher: $\alpha \sim 0.25$



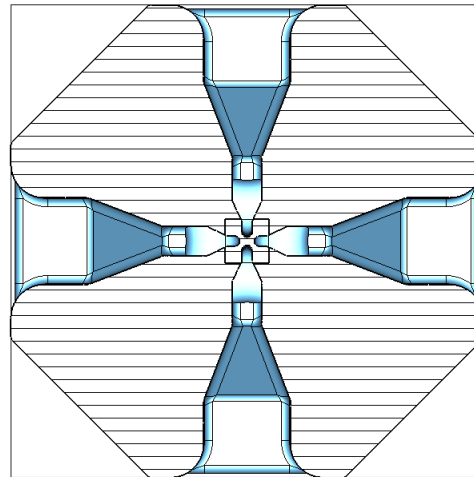
Emittance growth in LEBT reduced from 50% to 10%



176 MHz CW RFQ: EM Design - Full CST Model with Modulation



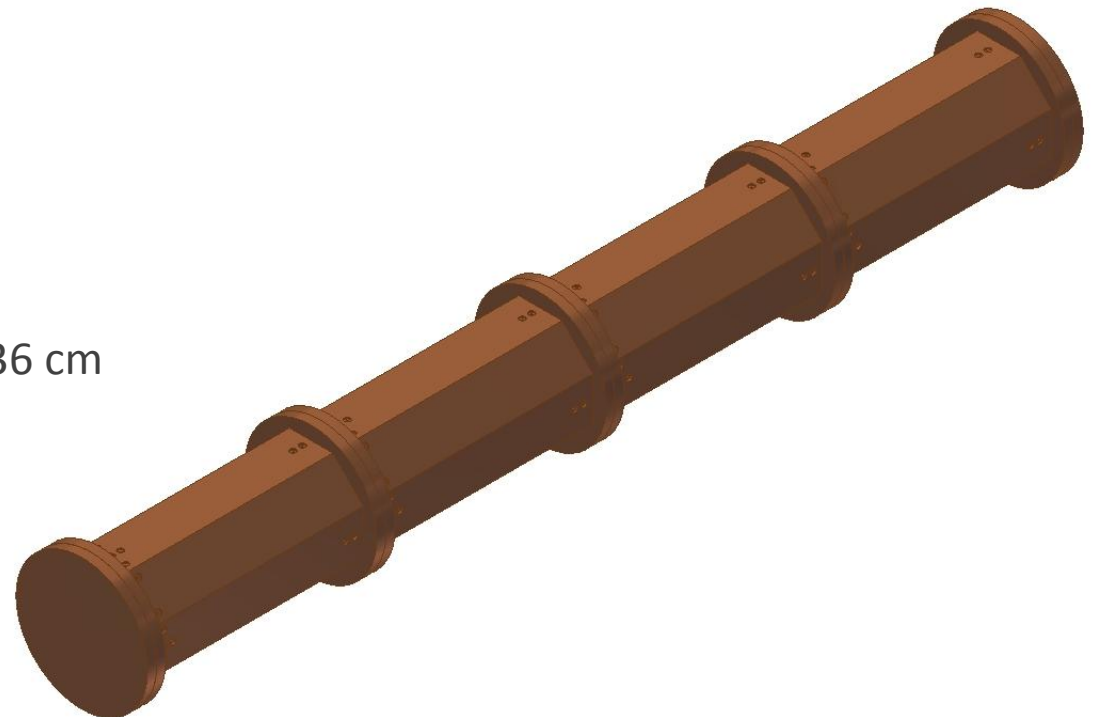
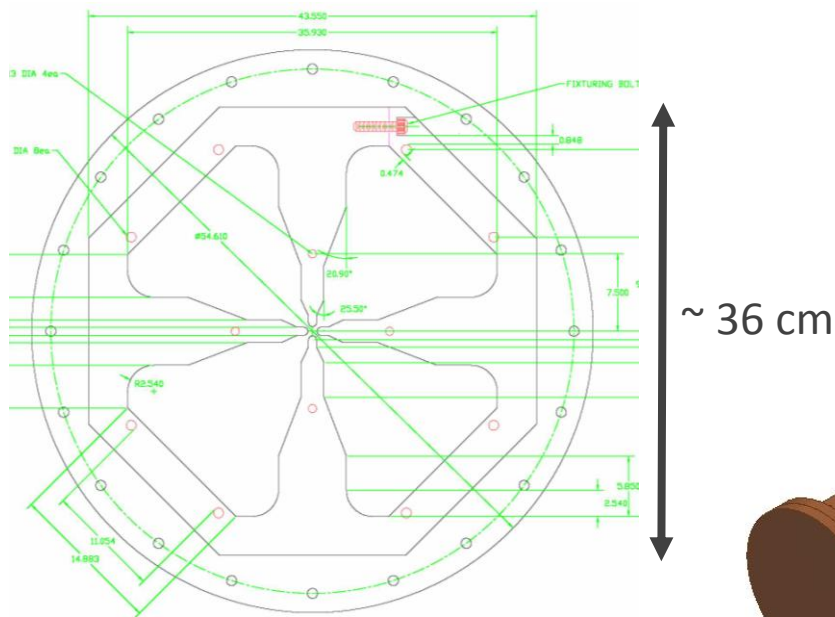
Parameter	Value
Frequency, MHz	176.0
Voltage, kV	75
Power Loss, kW	115
Q-Factor	13900



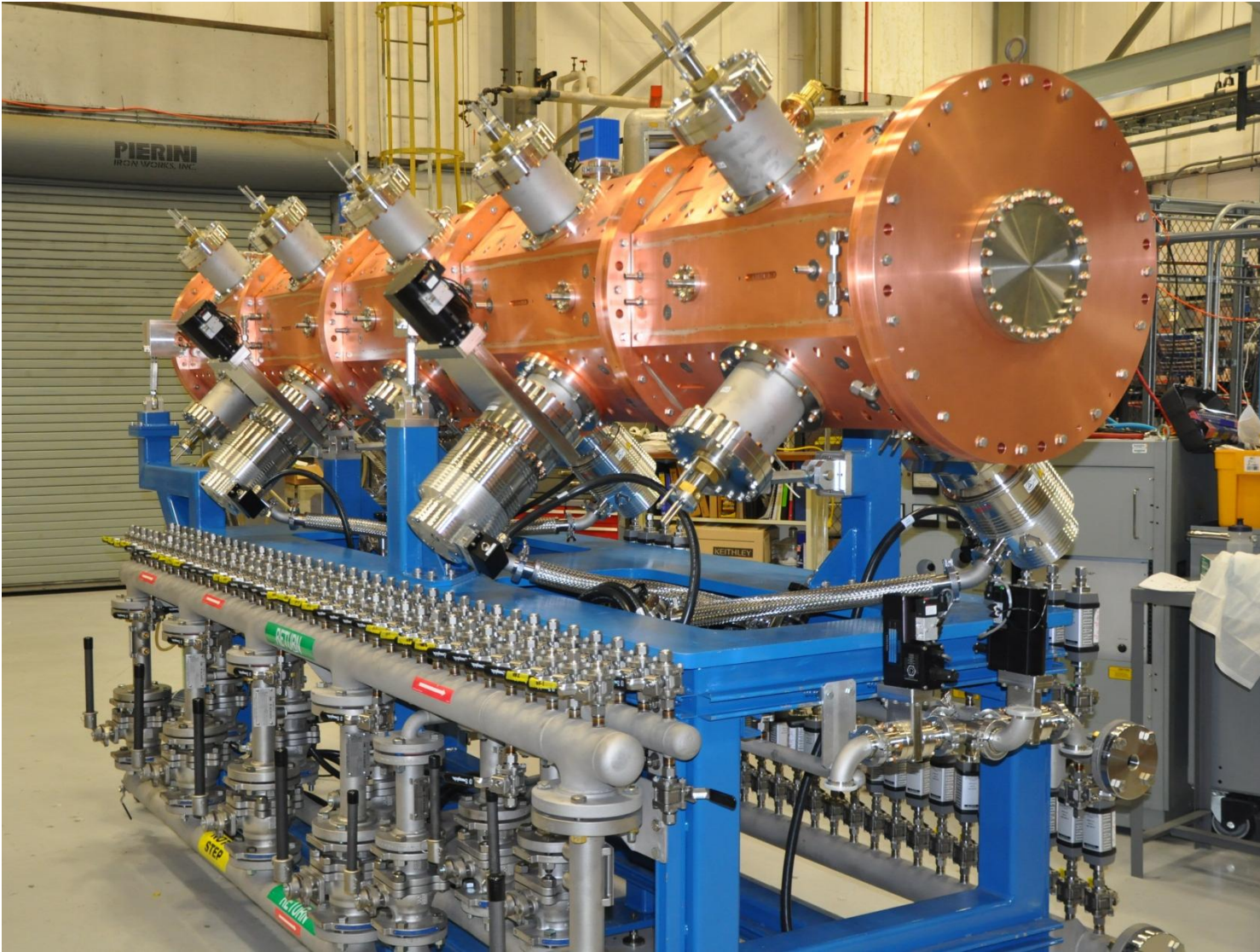
Mode	Frequency, MHz
Dipole Mode	172.9
Main Mode	176.0
Next Mode	178.7

176 MHz RFQ: Engineering Design & Fabrication

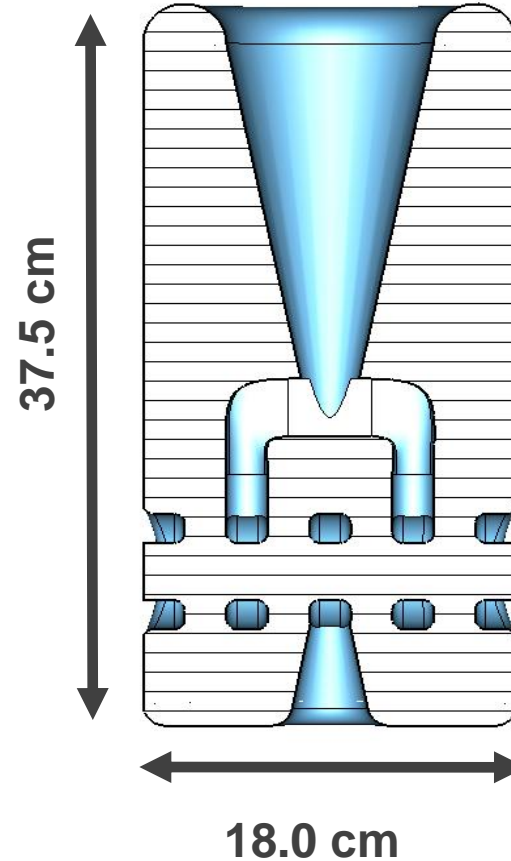
- 4-vane, 4-segments, 3.8-meter long
- OFE copper, furnace brazed in hydrogen atmosphere
- RF Power consumption – 115 kW (MWS), Voltage =75 kV
- The same technology as for the ATLAS Upgrade RFQ
- Transverse dimensions are smaller than the ATLAS RFQ by $\sim 15\%$



Proven & Always Improving Technology

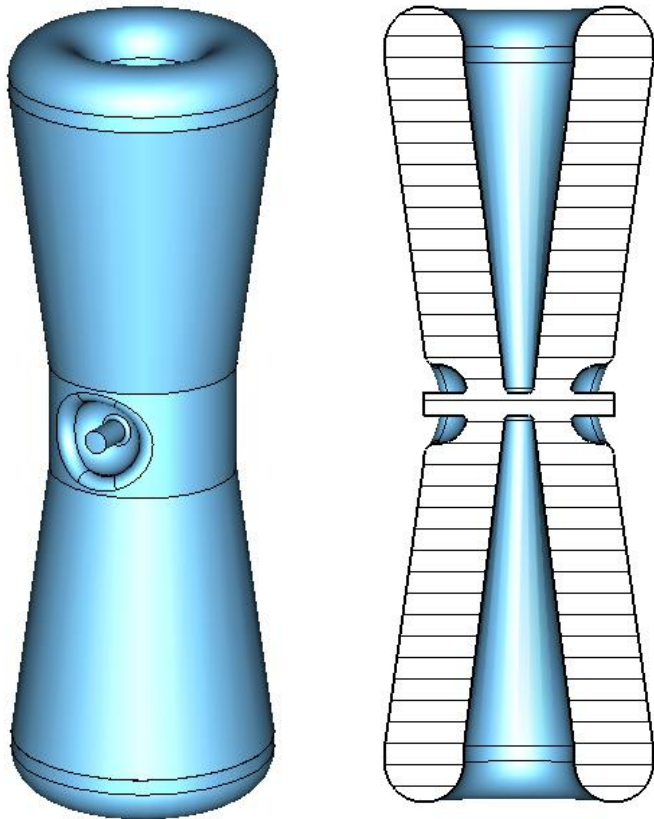


176 MHz Room Temperature Rebuncher: 4-Gap QWR



Aperture diameter – 30 mm
Voltage – up to 160 kV
RF power – 3 kW

EM Design Optimization: Fully Parameterized Geometry



Name	Value	Description
CVAPR	1.5	Cavity Aperture Radius
CVFL	2.0	Cavity Flat Length
CVMH	7.0	Cavity Middle Height
CVMR	12.0	Cavity Middle Radius
CVTBR	$(CVTR-ICTR)/2.0$	Cavity Top Blending Radius
CVTH	50.46	Cavity Top Height
CVTR	17.0	Cavity Top Radius
DTEBR	1.5	Drift Tube Edge Blending Radius
DTIBR	0.5	Drift Tube Inner Blending Radius
DTIR	5.0	Drift Tube Inner Radius
DTOBR	3.6	Drift Tube Blending Radius
DTOR	5.0	Drift Tube Outer Radius
DTPN	$CVMR-(MGD+GapW)/2$	Drift Tube Penetration
GapW	4.8	Gap Width
ICFL	2.0	Inner Conductor Flat Length
ICRTX	3.8	Inner Conductor Race Track Depth (X)
ICRTY	2.0	Inner Conductor Race Track Height (Y)
ICRTZ	$(MGD-GapW)/2$	Inner Conductor Race Track Width (Z)
ICTH	CVTH	Inner Conductor Top height
ICTR	7.0	Inner Conductor Top Radius
MGD	8.4	Mid-Gap Distance

Parameter List

Global

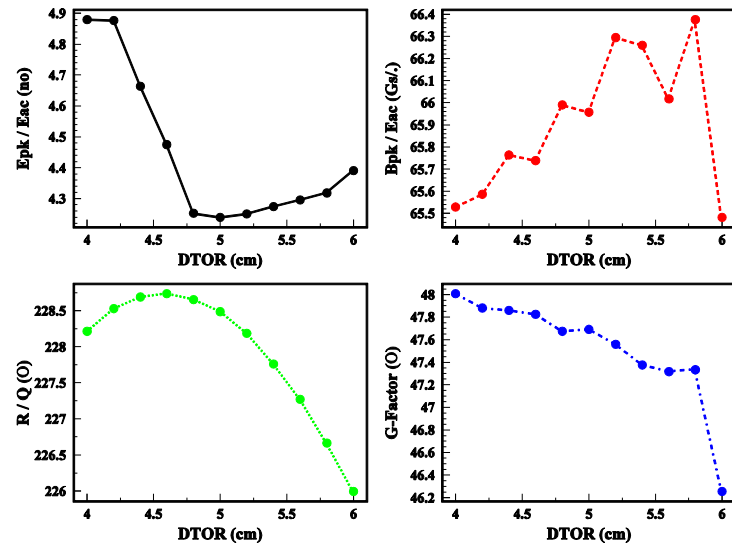
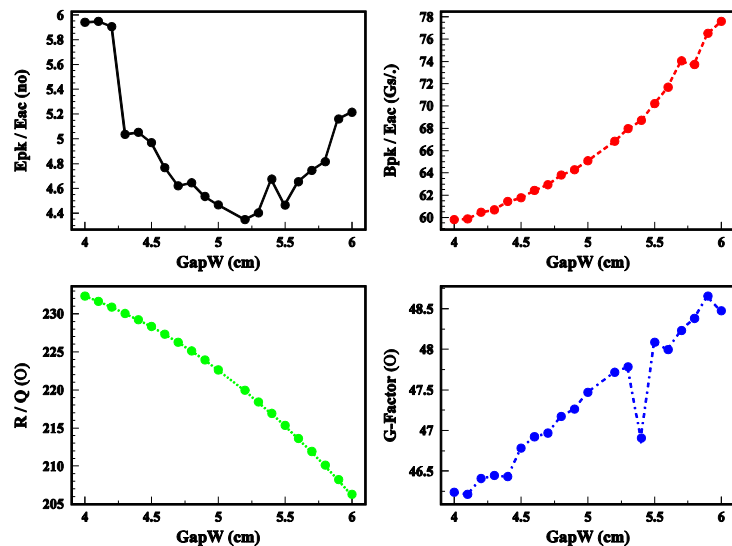
- The table shows the list of geometry parameters as seen in MW-Studio
- The geometry parameters are NOT independent

EM Design Optimization: RF Parameters to Optimize

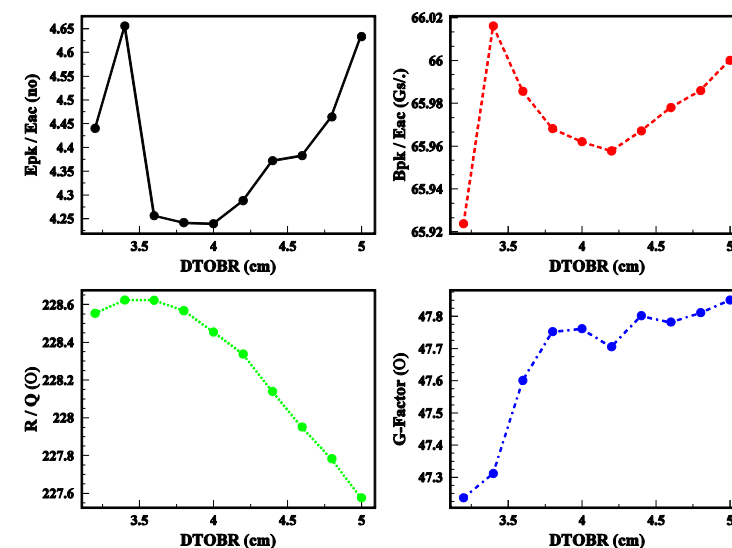
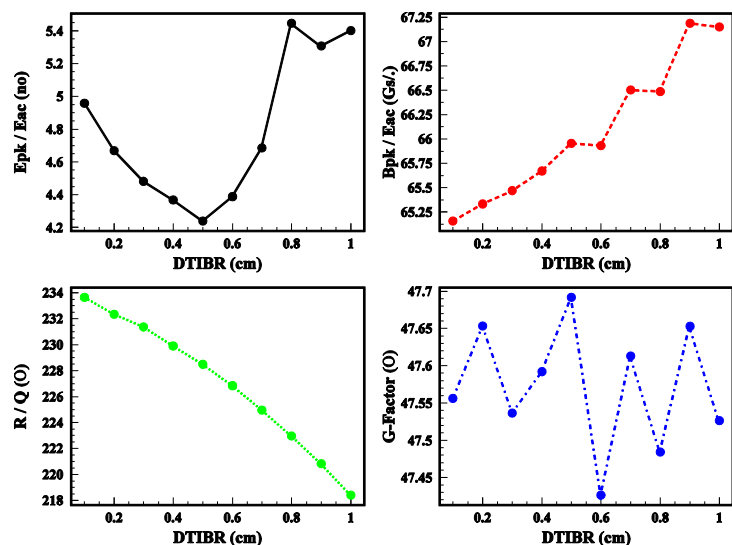
- **E-peak**: Minimize peak surface electric field to limit field emission
- **B-peak**: Minimize peak magnetic field to maintain superconductivity
- **$R/Q = V^2/\omega U$** : Maximize R/Q to produce more accelerating voltage (V) with less stored energy in the cavity (U)
- **$G = R_s * Q$** : Maximize the geometry factor to increase the cavity effectiveness of providing accelerating voltage due to its shape alone

EM Design Optimization: Parameter Sweeps in MWS

Gap Width



DT Inner Blend Radius

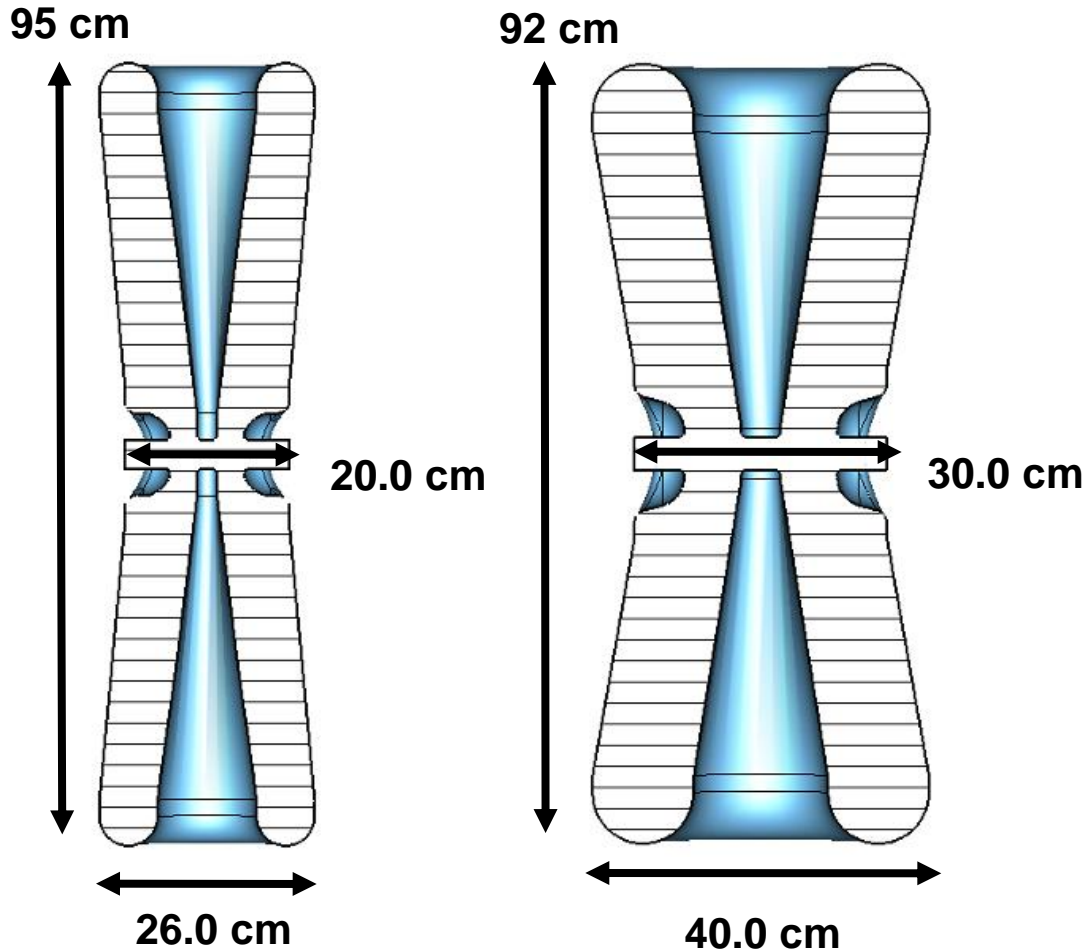


Drift Tube Outer Radius



DT Outer Blend Radius

Optimized Coaxial Race-Track HWRs: Some issues

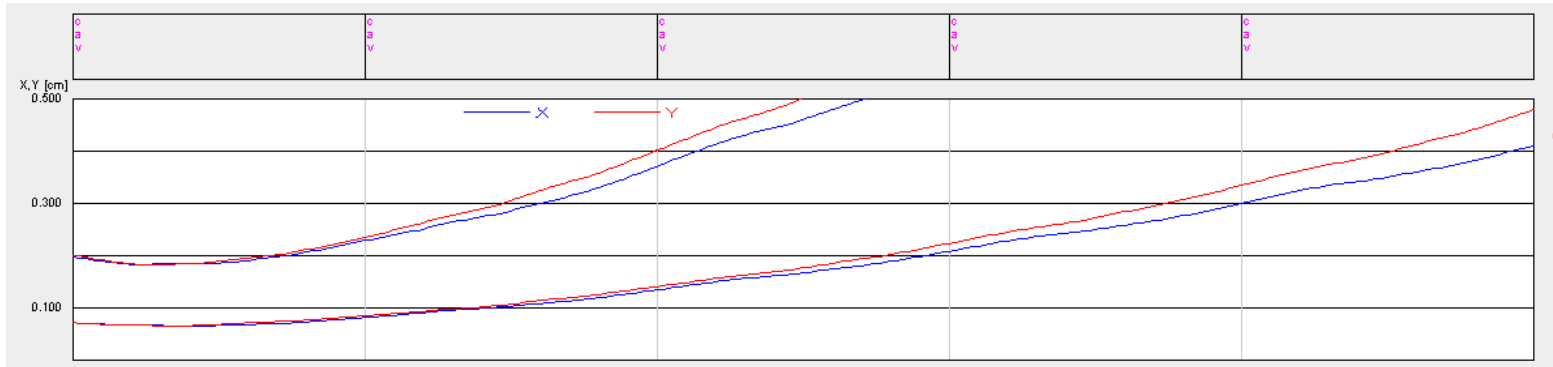


Cavity	Low- β	High- β
β_{opt}	0.087	0.16
L_{eff}	14.8	27.3
E_{peak}/E_{acc}	5.1	4.1
-		
B_{peak}/E_{acc} mT/(MV/m)	7.0	7.0
R/Q (Ω)	182	224
G-Factor (Ω)	40	60

- ✓ A Quadrupole field component causing beam asymmetry
- ✓ Peak surface magnetic field in the welding areas

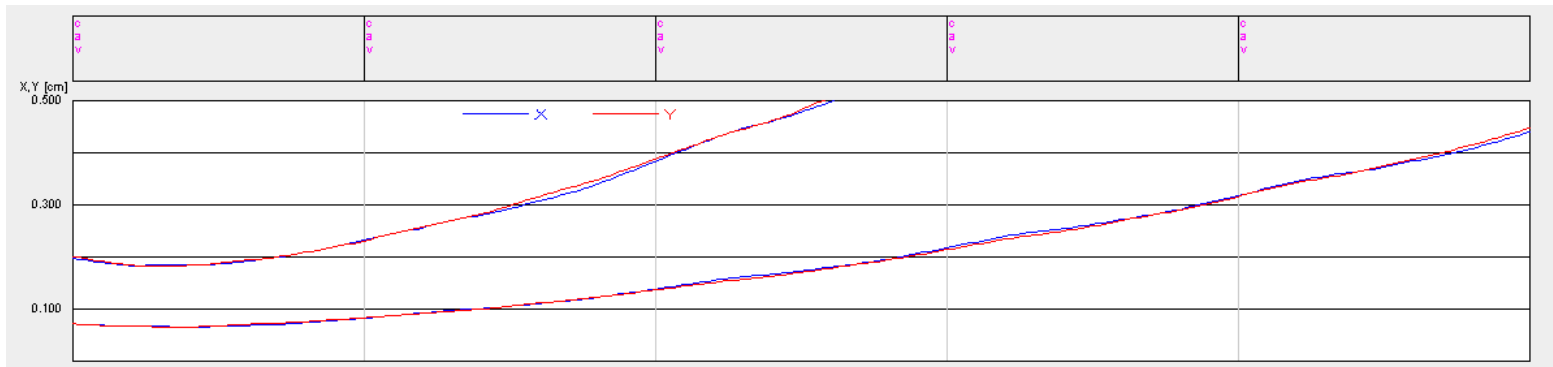
HWR Quadrupole Asymmetry Correction: Elliptical Aperture

Round Aperture



Asymmetry

Elliptical Aperture

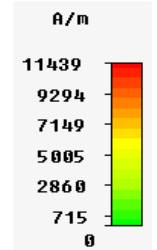
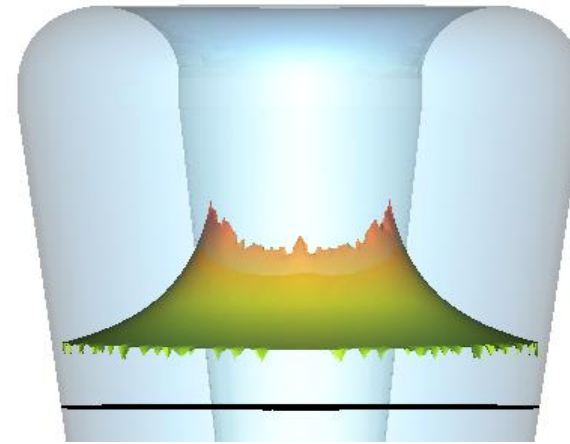
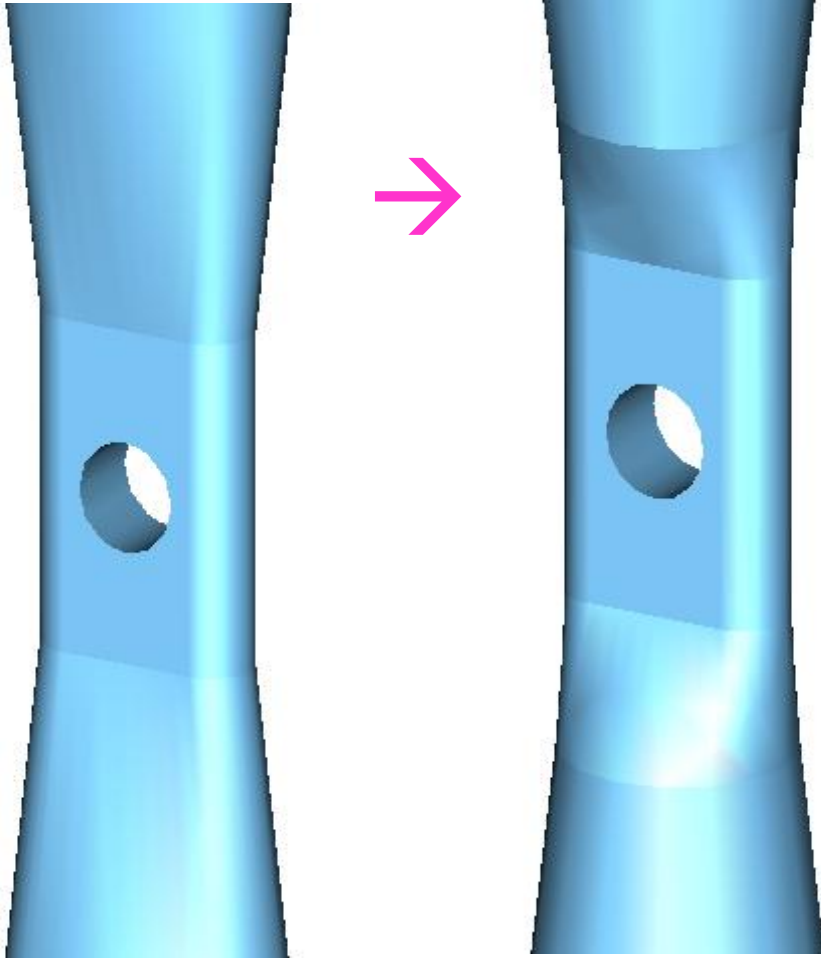


Asymmetry
Gone

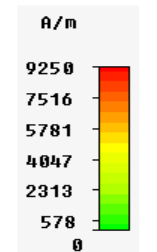
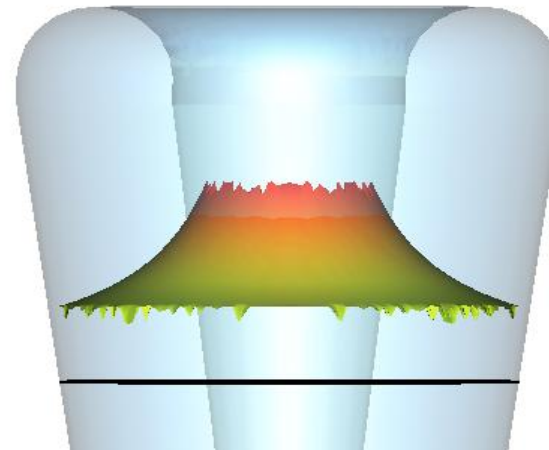
→ The required elliptical aperture is 33-36 mm for the low- β
and 36-40 mm for the high- β

For Uniform Magnetic Field: Round Loft in the CC

Race-Track Loft

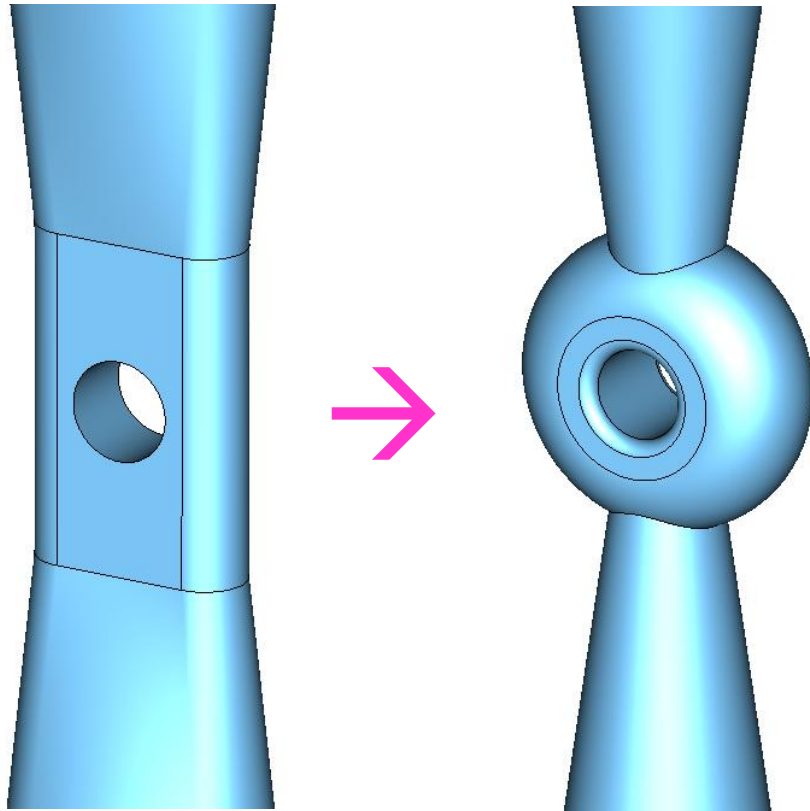


Intermediate Round Loft



The round loft re-distributes the magnetic field uniformly which also reduces the peak value

From Race-Track To Ring-Shaped “Donut” Center Conductor



Comparison for the SARAF High- β HWR
176 MHz – $\beta \sim 0.16$

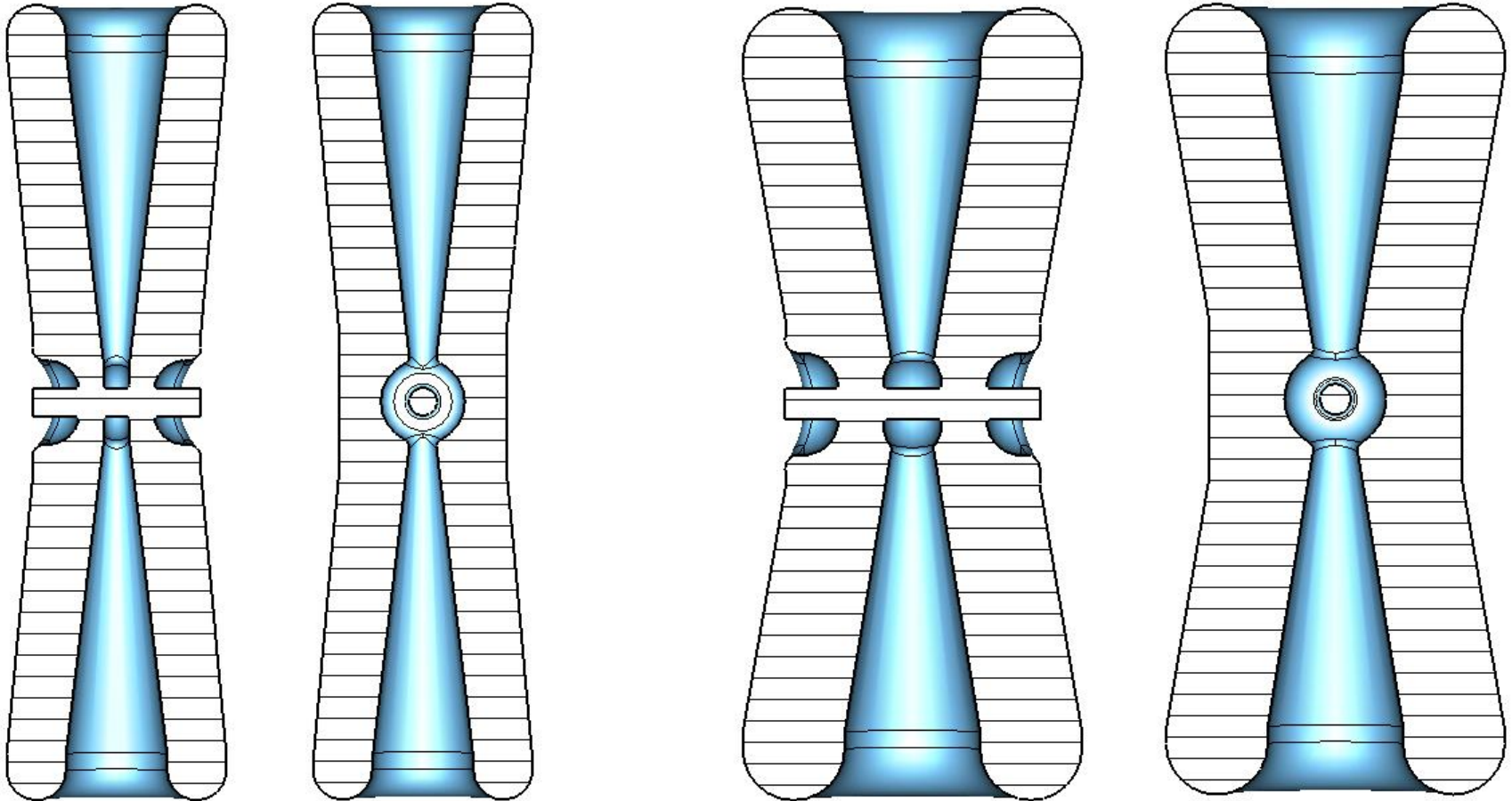
Cavity	Race-Track	Ring-Shaped	Diff. (%)
E _{peak} /E _{eacc} -	4.1	4.7	+14
B _{peak} /E _{eacc} mT/(MV/m)	7.0	5.6	-20
R/Q (Ω)	224	296	+32
G-Factor (Ω)	60	60	0

- ✓ 20% lower peak magnetic field → Farther from quench limit
- ✓ 30% higher shunt impedance → Same voltage with less power
- ✓ No quadrupole field component → No elliptical aperture needed

Optimized Ring-Shaped HWRs: Geometry

Low- β

High- β

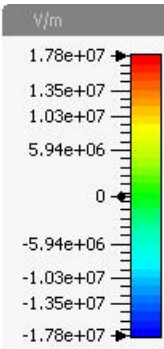
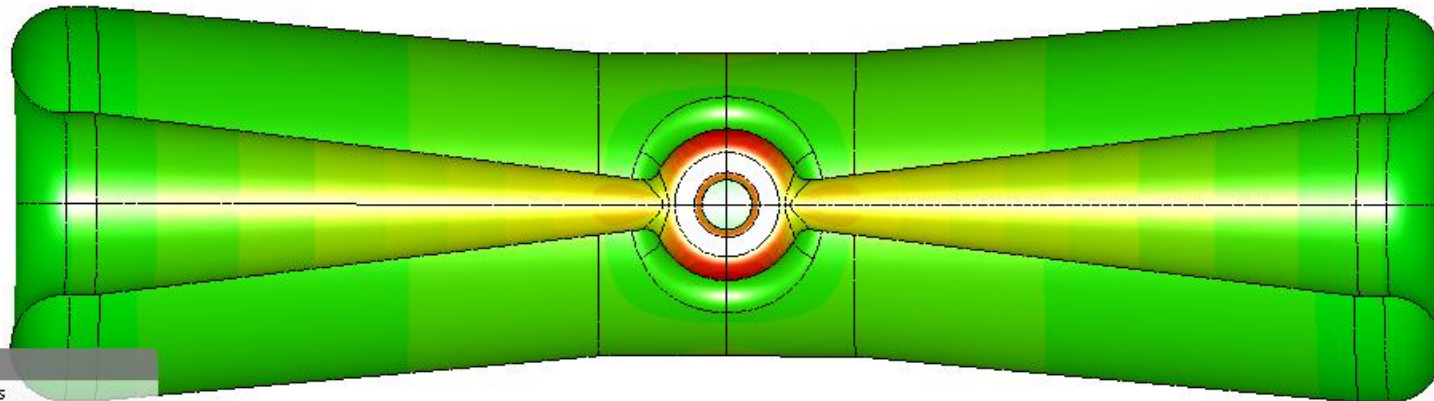


Optimized Ring-Shaped HWRs: RF Parameters

Cavity	β_{opt}	L_eff (cm)	E _{peak} /E _{eacc} -	B _{peak} /E _{eacc} mT/(MV/m)	R/Q Ω	G Ω
Low- β	0.089	15.2	5.3	5.6	231	40
High- β	0.16	27.3	4.7	5.6	296	60

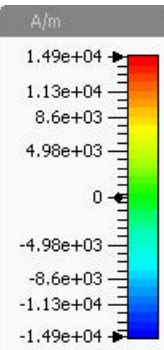
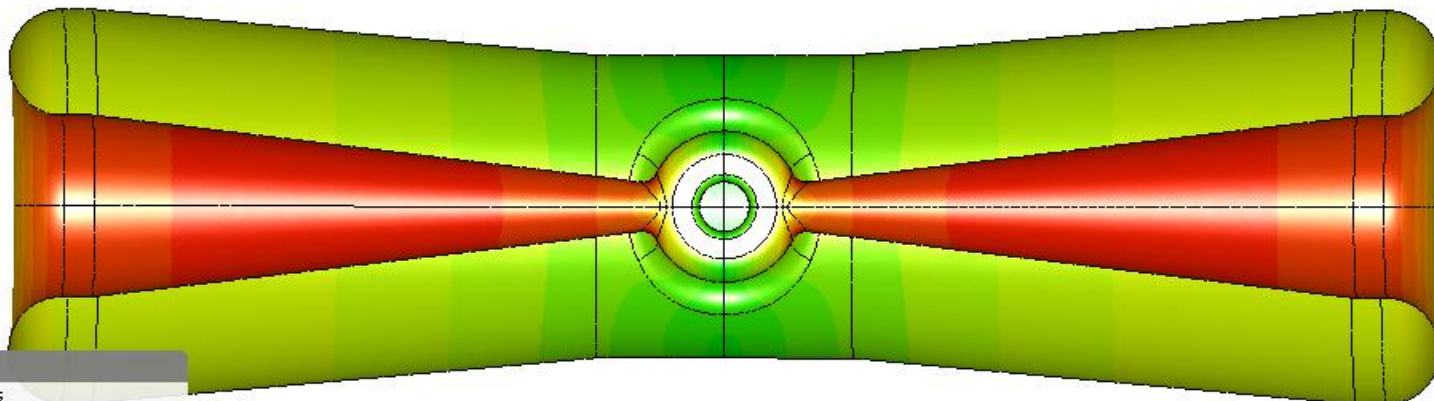
- The low- β HWR is capable of delivering 1.0 MV at 36 MV/m and 49 mT
or 1.5 MV at 51 MV/m and 70 mT
- The high- β HWR is capable of delivering 2.4 MV at 36 MV/m and 61 mT
or 2.7 MV at 41 MV/m and 70 mT

Low- β : Field Distributions



Mode 1 E (peak)

Component: Abs
Orientation: Outside
3D Maximum: 1.781e+07
Frequency: 176.014

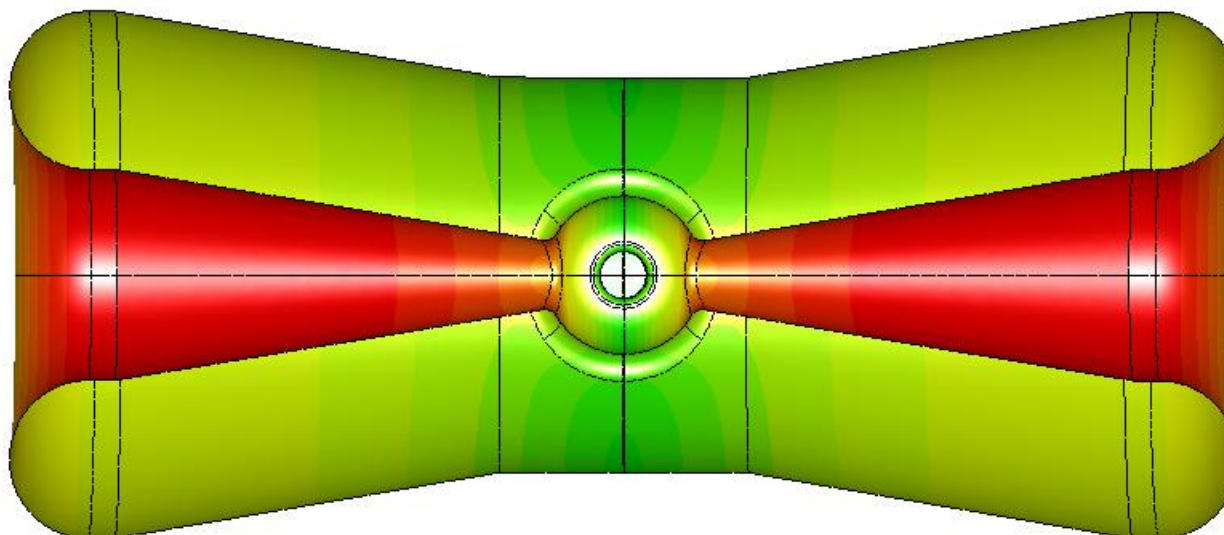
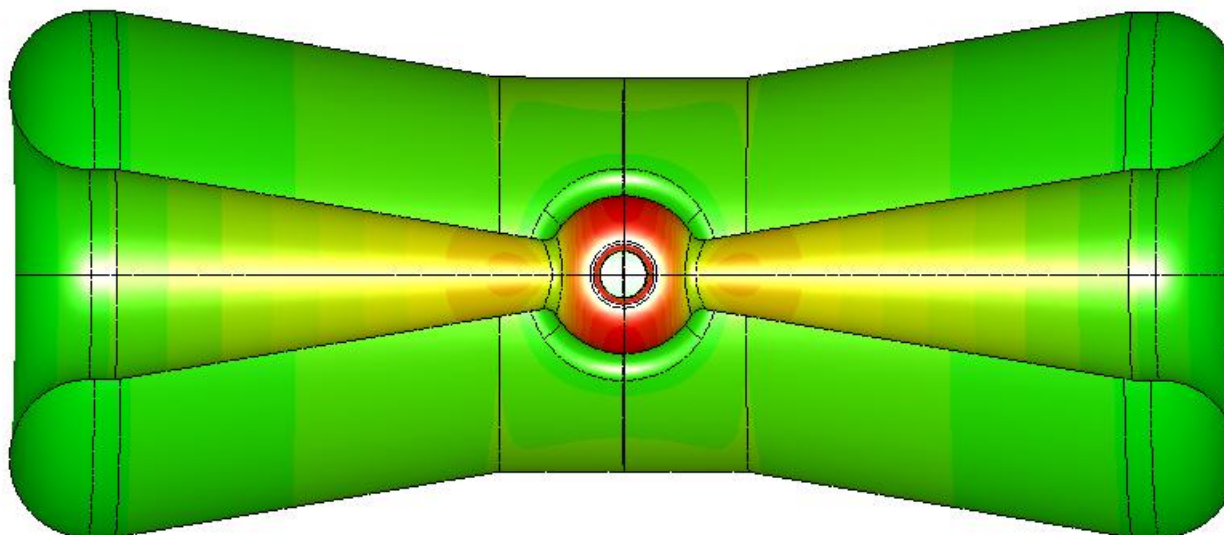


Mode 1 H (peak)

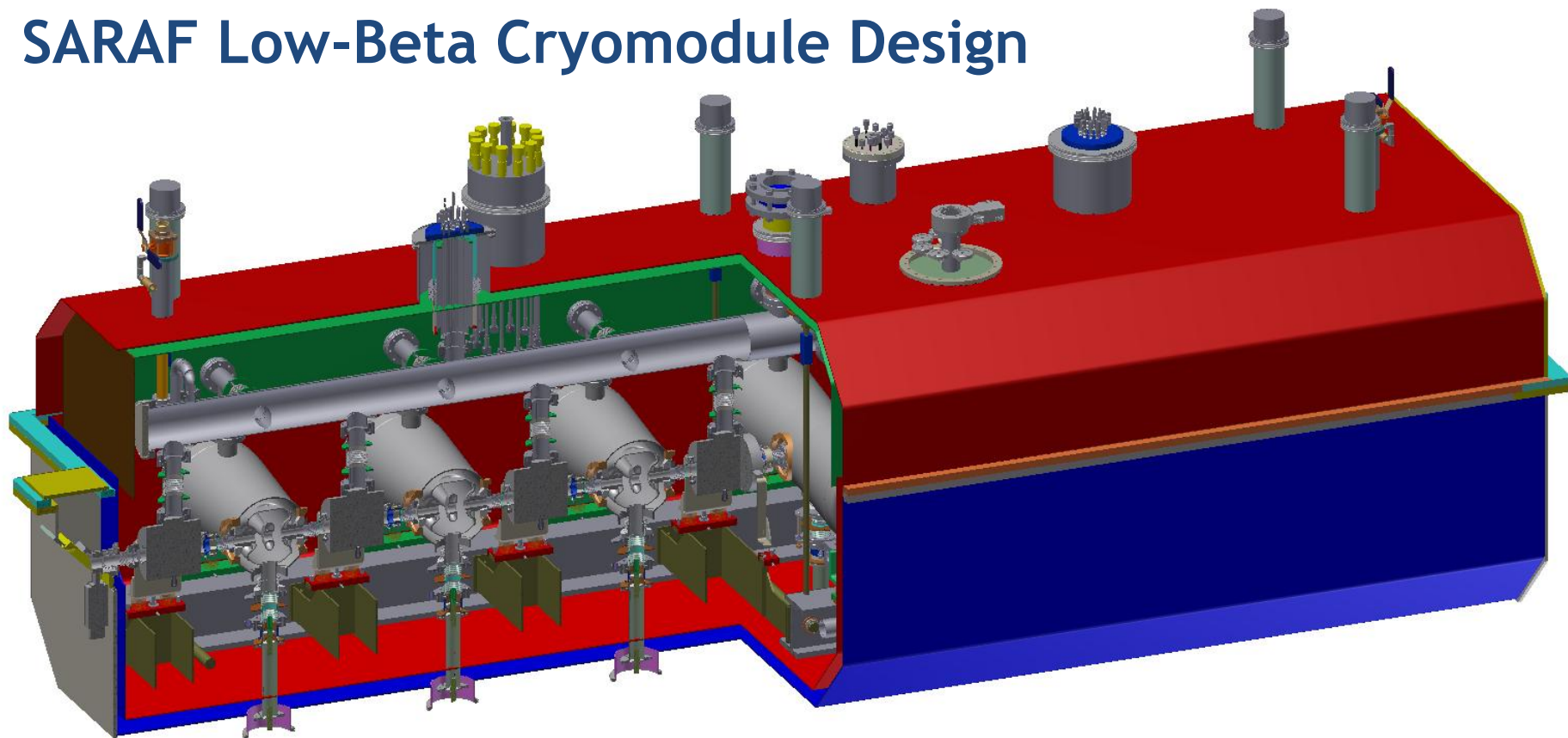
Component: Abs
Orientation: Outside
3D Maximum: 1.494e+04
Frequency: 176.014



High- β Field Distributions



SARAF Low-Beta Cryomodule Design

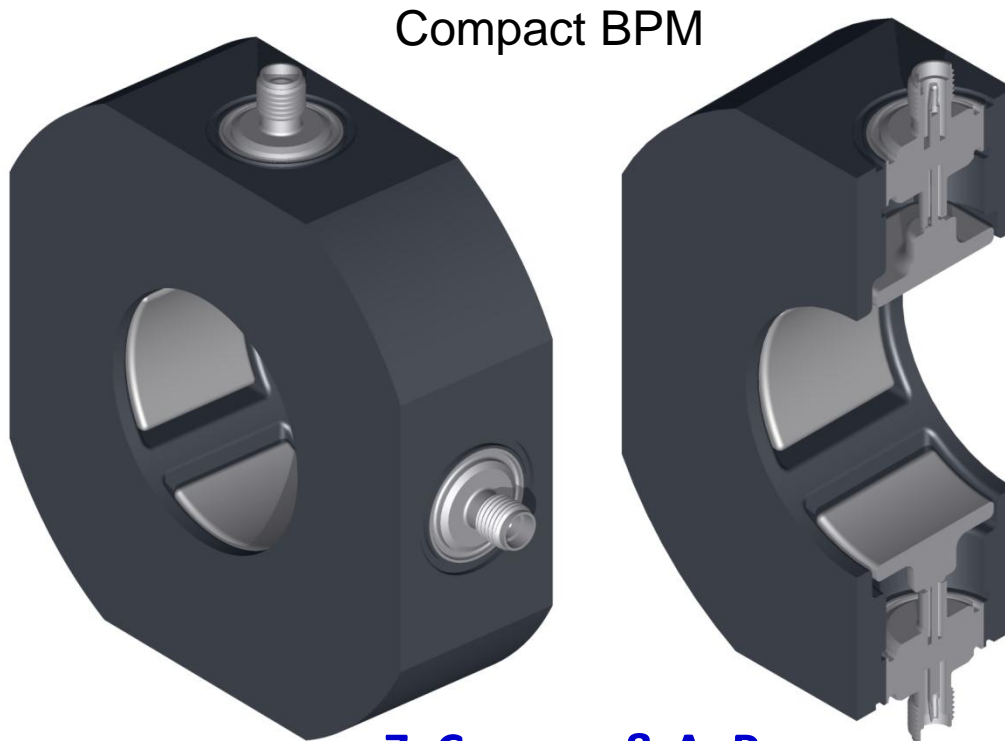


Parameter	Dimension
Cryomodule Width (m)	1.7 m
Cryomodule Height (m)	1.9 m
Cryomodule Length (m)	5.2 m

Z. Conway & G. Sherry

Compact Solenoid & BPM

- A combined 6 T solenoid and steering coil design is being developed in collaboration with Meyer Tool and Manufacturing and Cryomagnetics.
- Compact & cleanable BPM with 2.5 cm length. It is being built and will be tested later this year.



Compact BPM

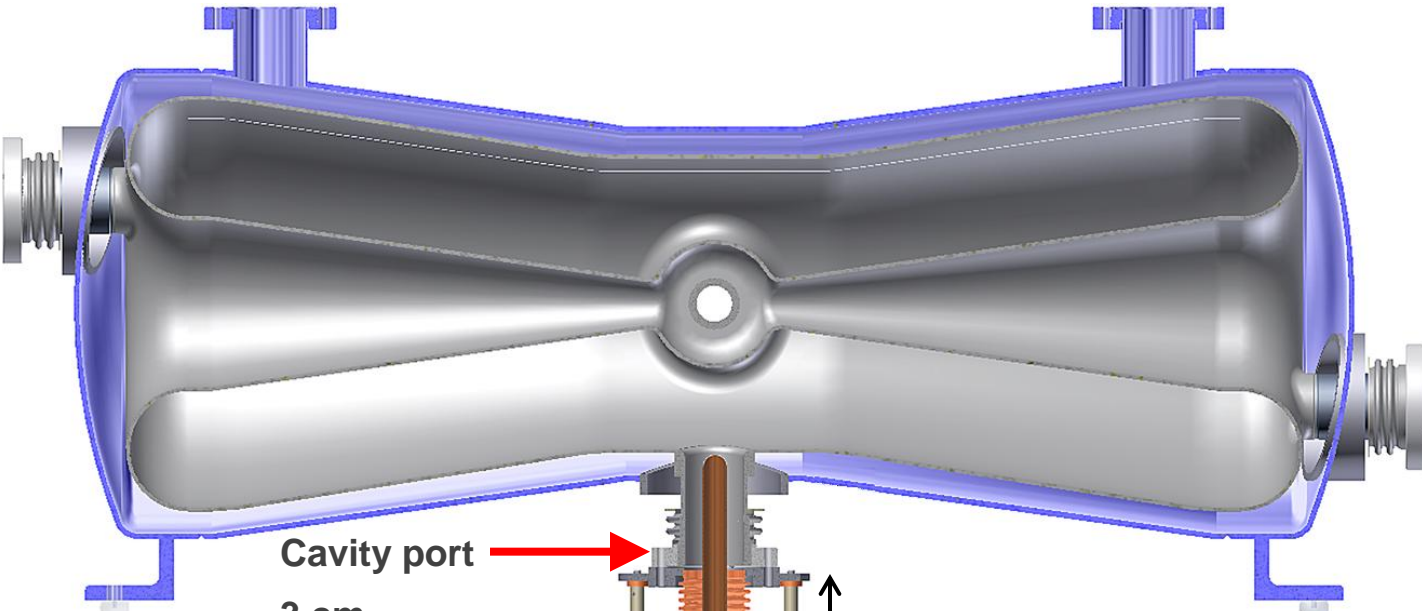
Z. Conway & A. Perry



M. Kelly

Assembly of beam spools,
solenoid, BPM and cavity.
Each unit = 0.64 m

A 15 kW CW Power Coupler for SARAF



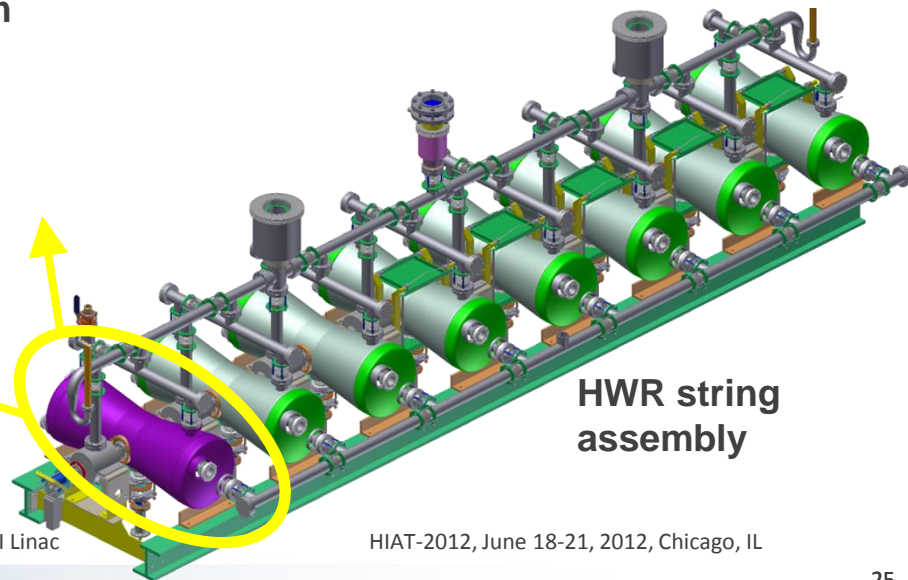
Cavity port

3 cm adjustable bellows

70 K 'cold' RF window

20 cm

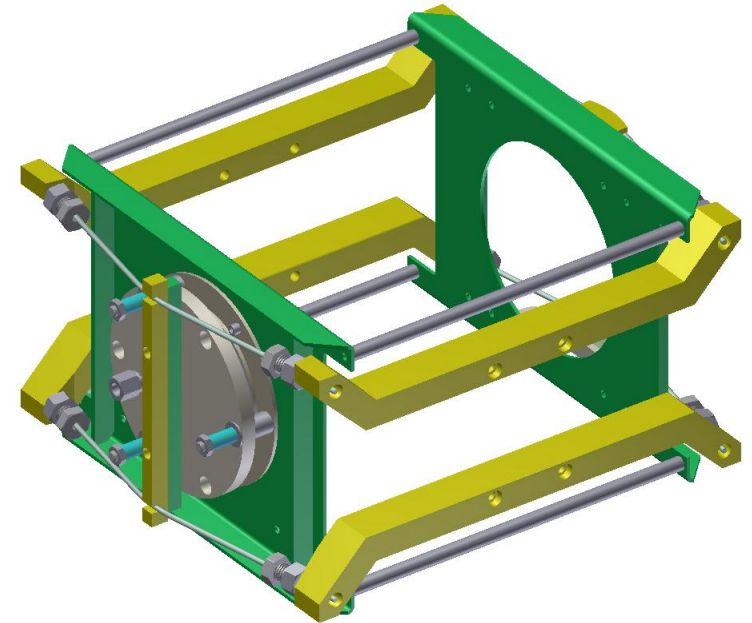
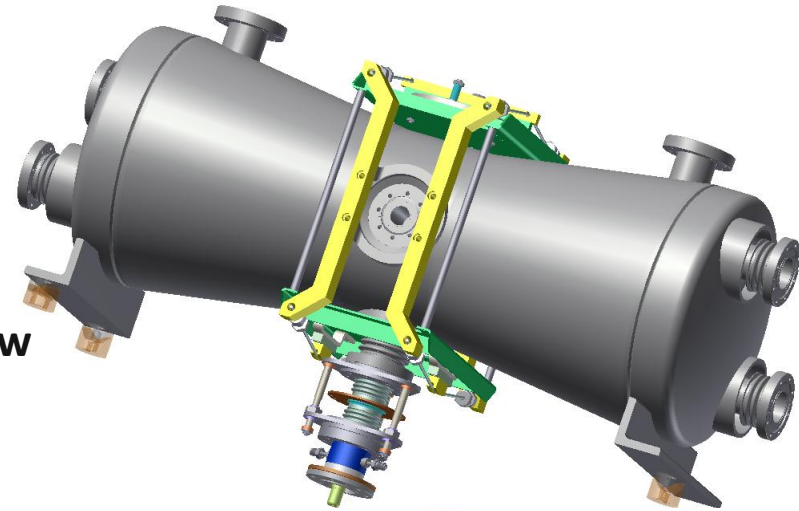
M. Kelly & S. Kutsaev



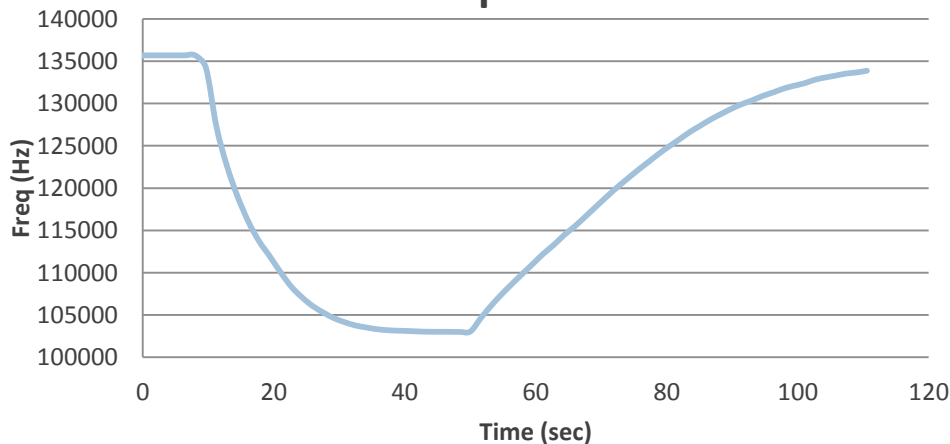
HWR string assembly

ANL Pneumatic Tuner Design

- No hysteresis.
- No backlash.
- No vibration; does not excite microphonics.
- Operates in a continuous feedback mode.
- Bellows is the only *moving part*.
- 109 MHz quarter wave cavity 32kHz tuning window
~1kHz / sec slew rate.
- Over 5×10^6 integrated operating hours with only 77.82 hours of downtime (downtime records are from 1994 to 2011).
- Can be easily applied for HWRs.



109 MHz QWR Measured Slow Tuner Response



Z. Conway & G. Zinkann

Beam-Line Alignment Tolerances

Dimension	Energy Upgrade	Intensity Upgrade	SARAF HWR
x (mm)	± 0.25	± 0.25	± 0.25
y (mm)	± 0.25	± 0.25	± 0.25
z (mm)	± 1	± 1	± 0.50
Pitch	$\pm 0.15^0$	$\pm 0.1^0$	$\pm 0.1^0$
Yaw	$\pm 0.15^0$	$\pm 0.1^0$	$\pm 0.1^0$
Roll	$\pm 0.5^0$	$\pm 0.1^0$	$\pm 0.1^0$

Results of Measurements with Beam

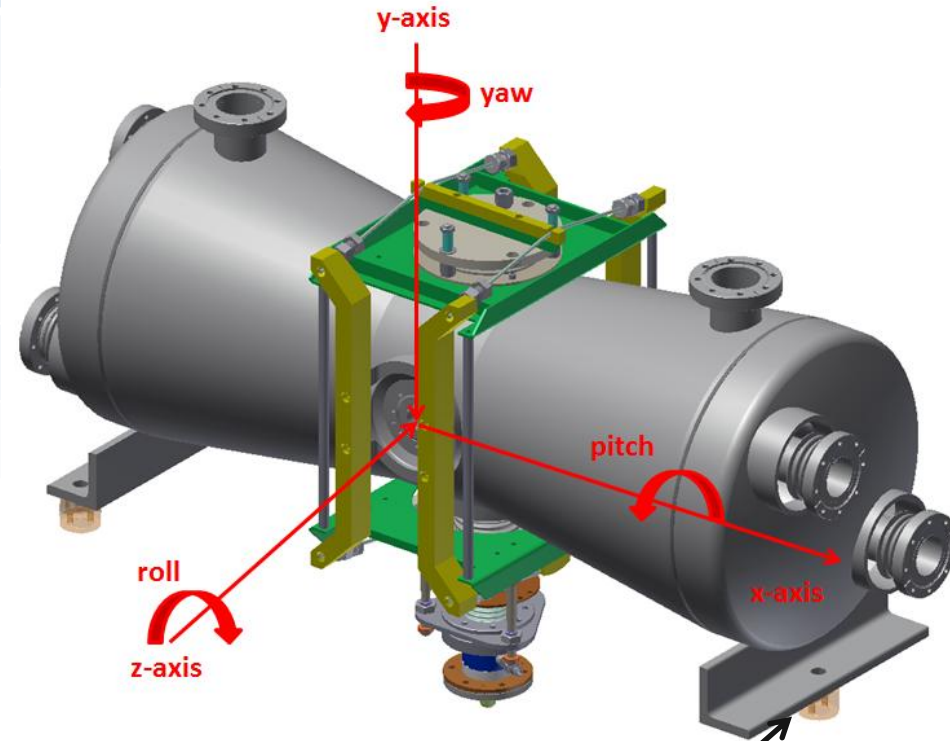
Alignment Hardware Examples



B. Mustapha

New Design for the SARAF Phase II Linac

Alignment Coordinate System



Alignment Puck (QNT 3)

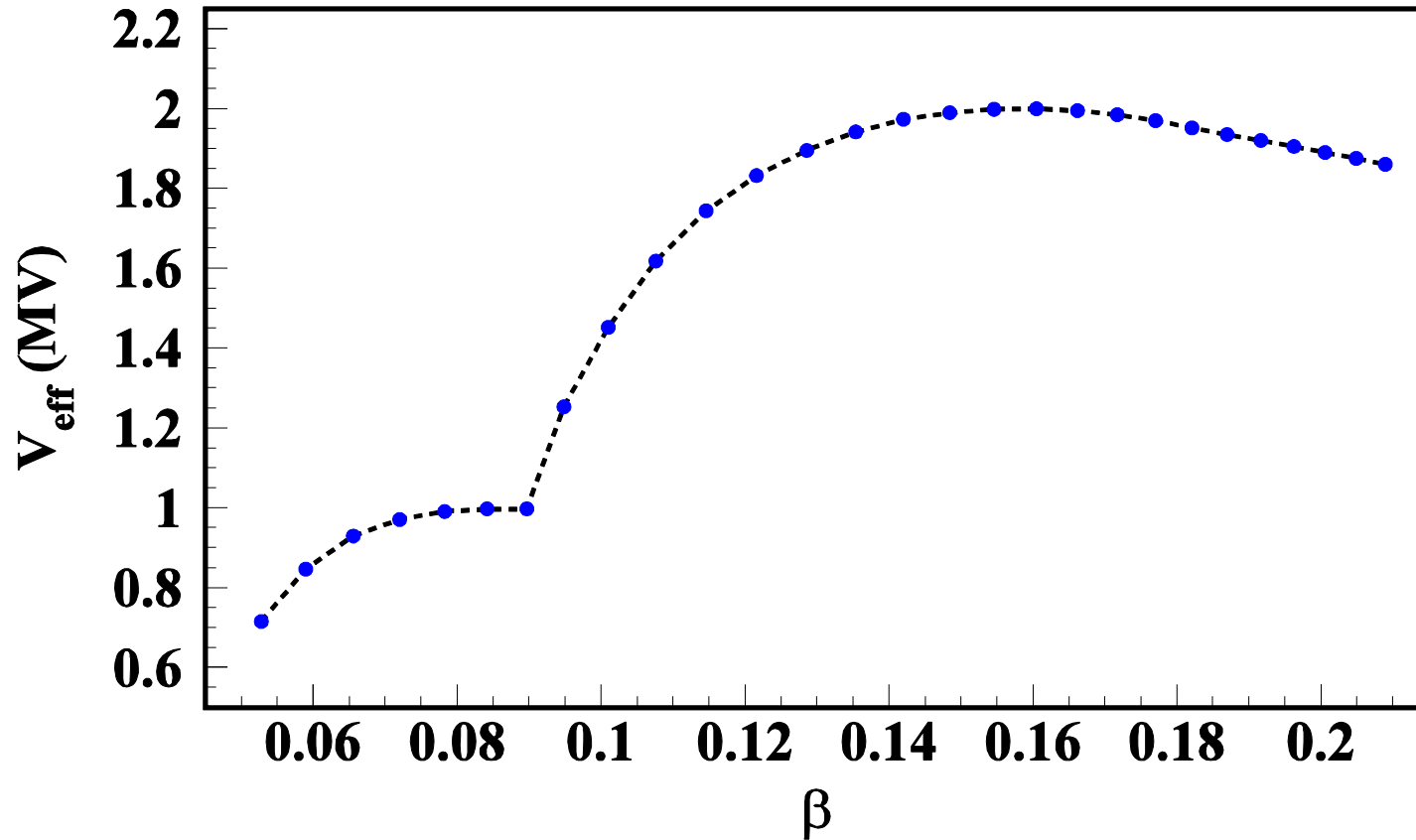
Z. Conway

HIAT-2012, June 18-21, 2012, Chicago, IL

New Linac Layout: Cavity Count

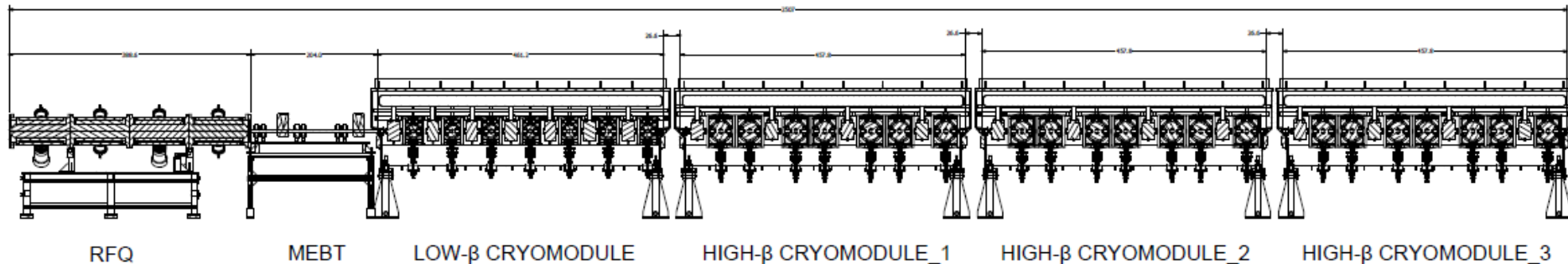
- To reach the desired beam energy of 40 MeV with nominal cavity voltage, we will need **7 low- β HWR at 1 MV**
and **21 high- β HWR at 2 MV**
- The cavities could easily outperform these nominal voltages
- For an adiabatic transition from the RFQ to the low- β section, the focusing period will consist of 1 cavity and 1 solenoid in the first cryomodule
- In the high- β section, the focusing period consists of 2 cavity and 1 solenoid except the last period in every cryomodule where we skip a cavity for better matching between cryomodules

Voltage Curve



New Linac Layout

- RFQ – 3.9 m
- MEBT - ~2 m
- Low- β cryomodule - 5.2m
- High- β cryomodule - ~5 m
- Total – 26 m

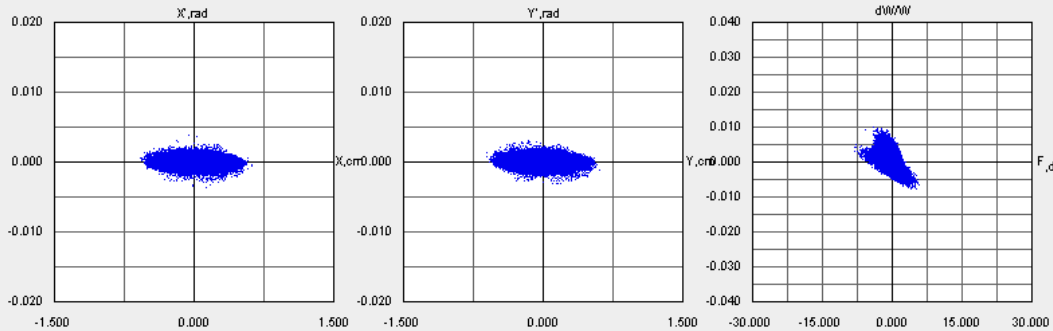


End-to-end Beam Dynamics: From the ECR ...

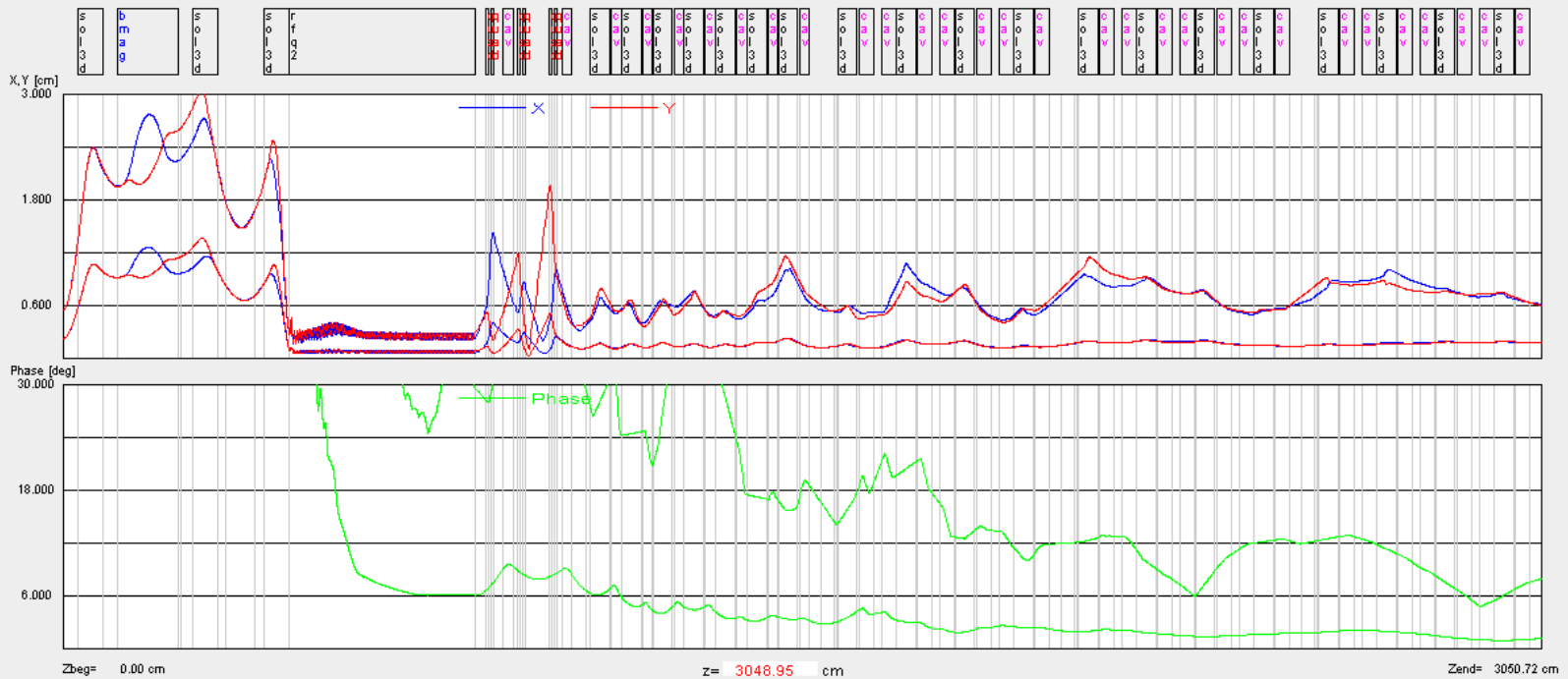
SARAF 176 MHz LINAC

Jun 18, 2012, 21:03:11

Jun 18, 2012, 07:18:06



Freq= 176.000 MHz
 W= 20.770 MeV/u
 Q= 1 e
 A= 2 AMU
 Npart= 99200
 Current= 4.960 mA
 SPACE CHARGE
 Nx= 32 Ny= 32 Nz= 64
 xylhSC= 1000.0 zlhSC= 1000.0
 hx/sx= 0.63 hy/sy= 0.61 hz/sz= 4.80
WARNING



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- Zachary Conway
- Michael Kelly
- Sergey Kutsaev
- Peter Ostroumov
- Gary Zinkann
- Andrei Kolomiets (ITEP – Moscow)
- Amichay Perry (Soreq NRC, Israel)
- Jacob Rodnizki (Soreq NRC, Israel)
- Dale Schrage (TechSource)
- Kenneth Shepard (TechSource)
- ...